Mansoura Engineering Journal

Volume 6 | Issue 2

Article 2

7-17-2021

Gap-Factor Approach in Non-Uniform Field Air Caps.

N. Farrag

Electrical Engineering Department., College of Engineering., Suez Canal University., Port-Said.

Follow this and additional works at: https://mej.researchcommons.org/home

Recommended Citation

Farrag, N. (2021) "Gap-Factor Approach in Non-Uniform Field Air Caps.," *Mansoura Engineering Journal*: Vol. 6 : Iss. 2 , Article 2. Available at: https://doi.org/10.21608/bfemu.2021.184639

This Original Study is brought to you for free and open access by Mansoura Engineering Journal. It has been accepted for inclusion in Mansoura Engineering Journal by an authorized editor of Mansoura Engineering Journal. For more information, please contact mej@mans.edu.eg.

GAP-FACTOR APPROACH IN NON-UNIFORM FIELD AIR GAPS BY Dr. N.M. FARRAG

ABSTRACT:

Method to determine the sparkover voltage for various gap geometries is described. The results indicate that a numerical coefficient of an empirical nature such as gap factor can be developed.

INTRODUCTION:

Gap-factor is a numerical device which describes the geometery of any particular configuration. Because of the time and expense involved in high-voltage tests on large structures, any method of extrapolating the known results is economically valuable and of a considerable aid to design. This powerful technique has been developed by Paris¹. Leroy, Gallet, Kosztaluk, and Kromer⁴ have been suggested that, the experimental determination of the gap-factor for any configuration at one spacing enables the well-established rodplane data to be extrapolating for that configuration for other spacings. This paper reports experiments for both positive lightning and switching impulses to represent the sparkover voltage of the air gaps by numerical calculation of the gap-factor for different geometries, e.g. rod-plane, toroid-plane, and sphereplane air gap configurations. The plane electrode was earthed. Gap lengths of 150 mm, 300 mm were attempted.

EXPERIMENTAL PROCEDURES

APPARATUS

A six-stage impulse generator of maximum output 330 kV was used to generate both lightning and switching positive impulses (1.2/50 µS and 60/2500 µS impulse shape respectivily). Gap lengths of 150 mm and 300 mm were attempted. The gap configurations were a hemispherically tipped rod of 19 mm diameter against an earthed plane, a toroid of 30 cm diameter against an earthed plane, and a sphere of 75 mm diameter against an earthed plane. Sparkover probability measurements were obtained from 50-60 impulses at each test voltage level. Fig. 1, shows the experimental arrangement for a rod-plane gap.

Suez Canal University, College of Engineering, Dept. of Electrical Engineering, Fort - Said.

E.16. N.M. Parrag

RESULTS AND DISCUSSION:

Gap-factor decreases with increasing divergence of the electric field distribution and increases with increasing convergence as shown in Figure 2 for both positive lightning and switching impulses. Similar results were obtained by Gallet³ for gaps up to 10 m. He showed experimentally for rod-rod gaps up to 10 m that the gap-factor was given by:

$$K = 1 + 0.6h/(h + d)$$

Where K was the gap-factor, h was the length of the earthed red, and d was the gap length. Figure 2, shows also that, the mean sparkover gradient increases linearly with increasing the gap-factor. The linear variation of spakover gradient with gapfactor was also found for more complex structures (Paris and Cortina⁴) Paris¹ (1967) propsed an empirical formula for rodplane gaps for positive switching impulses was given by:

$$V_{-} = G d^{n} k V (Paris^{1})$$

Where V was the sparkover voltage. He reported data obtained

with an impulse shape 120/4000 µS for longer gaps of up to 6.8m length. The parameters G, and n were 500 and 0.6 respectively. These parameters were 400 and 0.75 with great satisfaction with the experimental results obtained for the various gap configurations under investigation. It was found from the results that; the ratio of the positive switching-impulse sparkover voltages for dissimilar configurations was independent of the gap length. By taking as a base the sparkover voltage for the rod-plane gap configuration, which can be empirically represented(± 5% ervor)by:

$$V_{a} = 400 d^{0.75} kV$$

~ ~~

for positive lightning impulses and approximately, also valid for positive switching impulses.

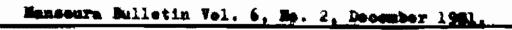
The sparkover voltage for any other configuration (V_s) can be given by:

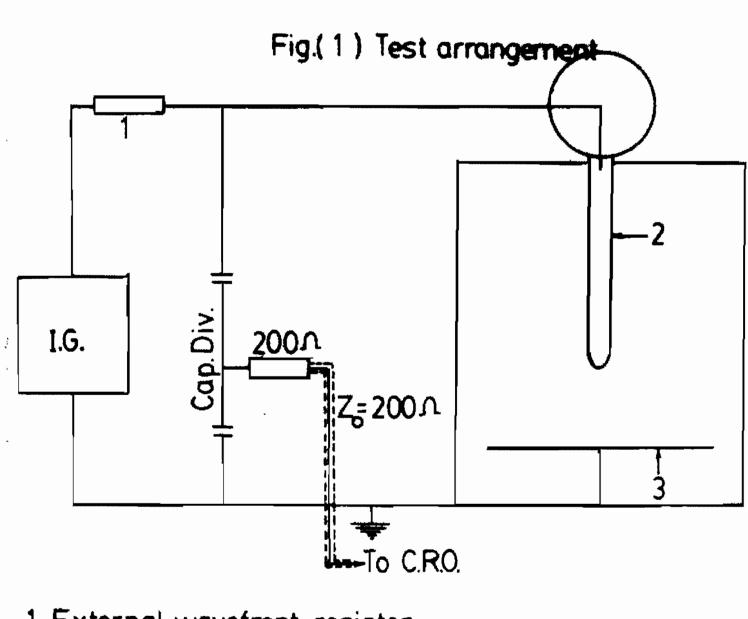
 $V_{g} = 400 \text{ K d}^{0.75} \text{ kV}$

where K is the gap factor for that configuration, and d is the gap length in meter. It is not possible to determine the gapfactor from the electrostatic field distribution, or to relate it to the physical development of the discharge (some useful attempts have been made by Schneider and Weck⁵; and Garcia⁶).

REFERENCES

 Paris, L. (1967). IERB Trans. PAS-86,936.
Leroy, G., Gallet, G.Kosztaluk, R., and Kromer, I.L.(1974). Rev. Gen. del' Electricité.
Gallet, G. (1974). Bull. CIGRE Group 33, Vol. II.
Paris, L. and Cortina, R. (1968). IEBE Trans., PAS-87,947.
Schneider, K.H., and Weck, K.H.(1974). Electra, No. 35, 25.
Garcia, H.N. (1975). Int. Symp. Hochspannungstechnik. Zurich.





- 1 External wavefront resistor
- 2 High-voltage electrode
- 3 Earthed plane electrode

