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SELF ADJUSTING DIGITAL CONTROLLER FOR AIRCRAFT SYSTEMS

## تحكم الطائرة الرقمية ذاتية الضبط

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يقدم البحث طريقته لتصميم المحكمات الرقمية ذاتية الضبط التي تستخدم في التحكم في الطائرات لكي تتناسب مع تغير معاملات الطائرة التي تنشأ من تغير حالات الطيران . يتم التحكم بالقياس المستمر لمعاملات الطائرة التي تعتمد على حالة الطيران ومقارنة هذه المعاملات المقاسة بحيز نطاقي يخلق حول معاملات حالة طيران محددة . أي انحراف لهذه المعاملات المقاسة عن الحيز النطاقي يحدث اضطراب في دليل محكم الطائرة للحصول على دوال حساسية تستخدم هذه الدوال في ضبط معاملات التنفيذ الرجمية للمحكم والنظام المقترح مناسب للتطبيق على المحكمات الحقيقية وتصميم هذا المحكم يمثل امتداد للتصور المعطى في ( 1 ) .

ABSTRACT

The paper describes an algorithm for designing self adjusting optimal controller for digital aircraft control systems to cope with the variation of the aircraft parameters under different flight conditions. The aircraft parameters which depend on the flight condition are continuously measured. A deadband zone around each of the parameters of a presetting flight condition is initiated. Any deviation from these bands will individually perturb the controller reference for obtaining sensitivity functions. These sensitivity functions will be used to adjust the feedback parameters of the aircraft control system. The proposed technique is suitable for implementation on real world control systems. The design of the proposed control represents an extension for that concepts included in [ 1 ].

INTRODUCTION

Aircraft control laws have been designed with modern linear quadratic technique [2,3] appropriately tempered with

established classical design requirements. In this type of design, the quadratic optimization problem was formulated and solved at selected flight conditions under assumptions of noiseless, full state and continuous time feedback. The resulting control gains and dynamics were then simplified and approximated as functions of measurable nominal flight condition parameters to produce standard gain control laws. However, such a controller may fail to cope with every flight condition, because of the variation of the aircraft parameters .

Different techniques for designing robust aircraft controller complying with prescriptive range of flight condition are also proposed [4,5,6] . However, these techniques does not guarantee the stability of the closed-loop system when subjected to perturbations in flight conditions.

This paper introduces a technique using the parameter sensitivity functions , resulted from variation in flight conditions, for adjusting the parameters of control systems. The proposed technique does not require any system identification except for the controller. The method offers the possibility of adjusting the parameters of optimal or suboptimal control schemes which have been installed on real systems.

#### AIRCRAFT SELF ADJUSTING DIGITAL CONTROLLER

The longitudinal linearized dynamic equations of an aircraft for deriving self adjusting controller, may be written as:

$$\dot{y} = A y + B v \quad y(0) = 0 \quad (1)$$

$$v = v_r - K y \quad (2)$$

Where :

A , B and y are defined [7] as:

$$A = \begin{vmatrix} z_1 & 1.0 & z_3 \\ M_1 & M_2 & M_3 \\ 0 & 0 & -a_3 \end{vmatrix}$$

$$B = [ 0 \quad 0 \quad a_3 ] ,$$

$$Y = [ Y_1 \quad Y_2 \quad Y_3 ] ,$$

- $y_1$  the angle of attack ;
- $y_2$  the rate of pitch angle ;
- $y_3$  the incremental elevator angle ;
- $v$  the control input to the elevator;
- $v_r$  the step disturbance of magnitude  $k_r$ ,
- $K$  the feedback matrix.

The approximate functional descriptions for the coefficients of the matrix A ( $z_1, M_1, M_2, M_3, z_3, a_3$ ) vary from a flight condition to another but all coefficients have the form [6] :

$$P_1 = g ( q_0, Mach_0, C )$$

- Where :  $q_0$  is the dynamic pressure ,  
 $C$  is a small perturbation parameter  $0.13 < C < 2.0$   
 $M_1, M_2, M_3, Z_1$  dynamic coefficient (function of C)  
 $Mach_0$  is the mach coefficient  
 $a_3$  function of C and  $q_0$

Implementation of the proposed method is based upon:

- (1) Initiate presetting flight conditions  $q'_0$  and  $mach_0$  .
- (2) Define deadband zones around these conditions.

upperband

$$q_0 + \Delta q$$

$$Mach_0 + \Delta Mach$$

lower band

$$q_0 - \Delta q$$

$$Mach_0 - \Delta mach$$

where,  $\Delta q$ , and  $\Delta Mach$  are permissible changes that retain system stability when occurred .

- (3) If the flight condition exceed the permiseible changes , a step disturbance of variable size individually perturb the

controller reference of the system for obtaining sensitivity functions.

- (4) Using these functions the controller parameters are adjusted .

The value of the variable size input  $k_r$  is defined as [1].

$$k_r = 1 + K y_f \quad (3)$$

$$y_f = -(A - B K)^{-1} B k_r \quad (4)$$

This value keeps the final values of system independent of the feedback parameters  $K$  ,

Equations (1) and (2) when restated in phase variable form become:

$$y_i (s) = W_i (s) \cdot v(s) \quad \text{for } 1 < i < n \quad (5)$$

$$v(s) = k_r (s) - \sum_{j=1}^n K_j \cdot y_j (s) \quad (6)$$

Substituting equation (6) into equation (5) gives:

$$y_i (s) = x_i (s) \cdot k_r (s) \quad \text{for } 1 < i < n \quad (7)$$

$$\text{where } x_i (s) = \frac{W_i (s)}{1 + \sum_{j=1}^n K_j \cdot W_j (s)} \quad (8)$$

The sensitivity of variable  $y_i$  with respect to parameter  $K_j$  is then :

$$S_{K_j}^{y_i} = \frac{\partial y_i}{\partial K_j} = \frac{\partial x_i (s)}{\partial K_j} \cdot k_r + x_i (s) \cdot \frac{\partial k_r}{\partial K_j} \quad (9)$$

When this equation is expanded and restated in sampled form it becomes :

$$S_{k_j}^{y_i}(\alpha \cdot \Delta t) = \frac{1}{k_r} \left[ \sum_{\beta=1}^{\alpha} - \frac{y_i(\alpha \cdot \Delta t) - y_i((\beta-1) \cdot \Delta t)}{\Delta t} \right. \\ \left. y_i(\alpha \cdot \Delta t - \beta \cdot \Delta t) \right] + \frac{1}{k_r} \cdot y_{rj} \cdot y_i(\alpha \cdot \Delta t) \text{ for } 1 < \alpha < n_s \quad (10)$$

where :  $n_s$  = number of samples

$\Delta t$  = sampling interval

$y_i(0) = 0$  for  $1 < i < n$

The last equation can then be used in calculating the changes of the feedback parameters necessary to cope with the changes in flight conditions.

The time response of variable  $i$  after change  $\Delta K$  in the parameter matrix  $K$ ,  $y_i(t, K + \Delta K)$  is related to the time response before the changes,  $y_i(t, K)$  by the equation:

$$y_i(t, K + \Delta K) = y_i(t, K) + \frac{\partial y_i}{\partial K} \Delta K + \frac{\partial^2 y_i}{\partial K^2} \Delta K^2 + \dots$$

when higher terms are neglected this equation takes the form :

$$y_i(t, K + \Delta K) = y_i(t, K) + \sum_{j=1}^n \Delta K_j \cdot S_j(t) \quad (11)$$

It is then desired to compute the parameter changes  $\Delta K$  so as to minimize the difference between the responses after the changes and the target responses  $y_r(t)$ . This is accomplished by substituting the expression for  $y_r$  given by equation (4) for all  $i$ , into equation (11) instead of  $y_i(t, K + \Delta K)$ . A quadratic system performance index is defined in the form:

$$L = \frac{1}{2} \int_0^{\infty} (y_r - y) Q (y_r - y) + (v_r - v) T (v_r - v) dt \quad (12)$$

Where  $Q$ ,  $T$  are weighting matrices and  $y_r$ ,  $v_r$  are target responses to which it is required that the system outputs  $y$  and  $v$  should approach. The performance index  $L$  is minimized with respect to the parameter change  $K$  by differentiating  $L$  with

respect to each of the parameter changes in turn and setting the derivatives to zero:

$$\frac{\partial L}{\partial K_j} = 0 \quad \text{for } 1 < j < n \quad (13)$$

This process results in a set of  $n$  linear equations in the unknowns  $\Delta K_j$  for all  $j$ , and these are solved to obtain values for all the parameter changes  $\Delta K_j$ .

The algorithm can be summarized in the following steps.

- 1- Start with a feedback parameter  $K$  corresponding to any flight condition .
- 2- Define small variations in flight condition parameters that retain system stability when any is occurred.
- 3- Set flight condition parameters of the controlled system and create bands around these parameters(parameters  $\pm$  variation).
- 4- Measure system flight parameters .
- 5- Compare the current flight parameters with the upper and lower limits of the band .
- 6- If flight parameters are located inside the band go to step 4
- 7- Apply a step signal with a size given by equation (3) on the controller reference.
- 8- Use equation (10) to calculate the sensitivity functions resulted from variation in flight parameters.
- 9- From equation (13) calculate the necessary feedback parameters variations..
- 10- Update the feedback parameters of the aircraft controller.
- 11- If the performance index  $L$  is minimized go to step 3 otherwise go to step 7.

#### EXAMPLE

The proposed technique is used to optimize the performances of an aircraft control system under varying flight condition. The system is represented by equation (1). The elements of the matrix  $A$  are computed according to the flight conditions [6] while  $B$  is taken as  $[ 0 \quad 0 \quad 6.6667 ]$ . Five flight conditions are

assumed. Each of which is imposed for a period of fifteen seconds. These flight conditions are tabulated below:

FLIGHT CONDITION	1	2	3	4	5
$Mach_0$	0.4	0.67	0.67	1.2	1.2
$q_0$	109	109	305	305	395

The parameter variations  $Mach$  and  $q$  are defined as 0.05 and 25 respectively. The responses of the proposed control system are illustrated in figure (1). These responses show that the system is stable for all assumed flight conditions.

#### CONCLUSIONS

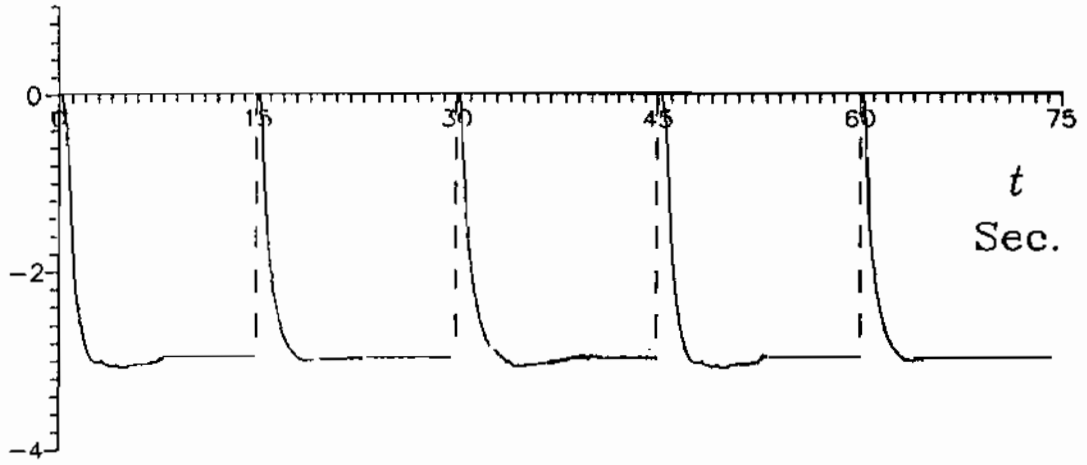
In this paper a method, based on parameter sensitivity functions, for designing self adjusting digital control systems has been described. This method does not require any parameter identification of the system except that of the controller. The method involves the use of parameter sensitivity functions for adjusting the parameters of an aircraft control system to follow the system dynamics. The technique is suitable for implementation on real world system.

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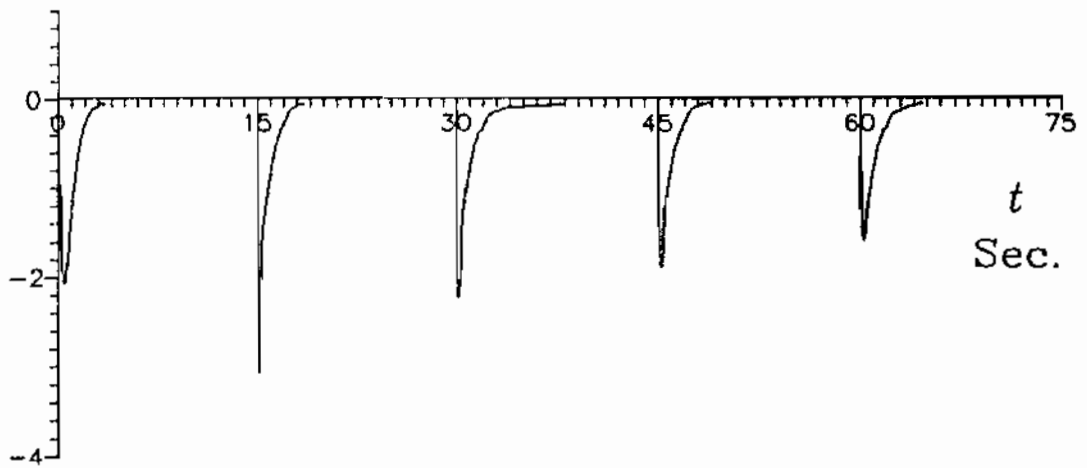
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THE RESPONSE OF THE P.U CHANGE  
OF ATTACK ANGLE X1



TIME RESPONSE OF THE P.U  
CHANGE OF PITCH ANGLE X2



THE RESPONSE OF THE P.U CHANGE OF  
INCREMENTAL ELEVATOR ANGLE X3

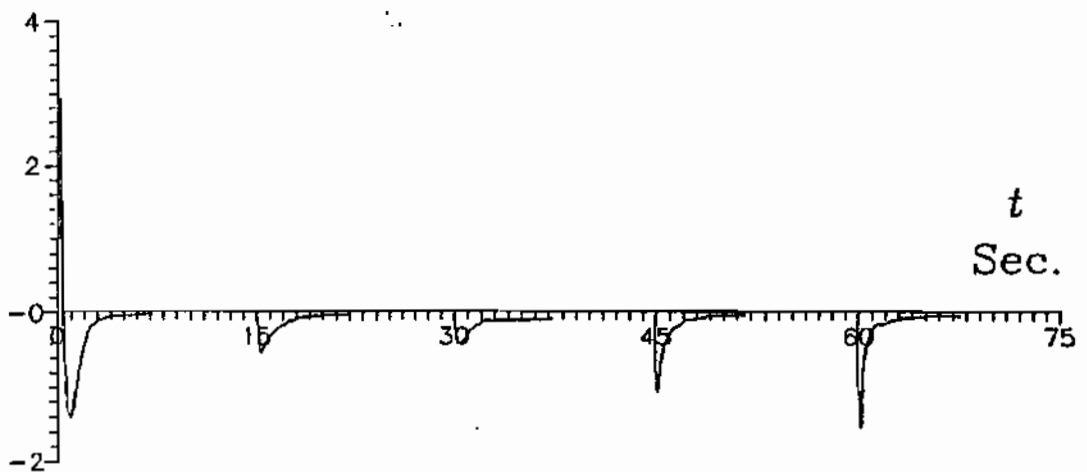


FIGURE (1): TIME RESPONSES OF THE CLOSED-LOOP CONTROL SYSTEM

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