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Sabry Saraya

Assistant Professor., Control and Computers Engineering Department, Faculty of Engineering., El-Mansoura University., Egypt., drsfsaraya@mans.edu.eg

Fayez Areed Associate Professor., Control & Computers Engineering Department., Faculty of Engineering., El-Mansoura University., Mansoura., Egypt.

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DESIGN OF A ROBUST ELECTRO-MECHANICAL CONTROL SYSTEM

عدوان البحث :- تصميم لاادون تحكم للمنظومة كهروميكاديكية

SABRY F.S AREED F.F.G Lecturer Associate Prof. Department of control and computers El-Mansoura University

جليفم اليهددي –

يلام البعدة طريلة ملترحدة لتصميم دلخام تعدكم لمنظومة كمروميكانيكية، و يعتوى البحث على النموذج الريدة لم لمنظومة كمروميكانيكية مكونة من محرك تيار معتمر محكوم من داغرة العلم السدوار و مولد تيار متردد ذو وجه واحد. و هذه المعظومة لها فرجان يتم التحكم ليهما و هما التردد و اللدرة الناخيتين من المولد ذو التيار المتردد و ذلك حتى يمكن ضبطهمنا لتغلاية محرك تيار متردد للتحكم في سرعته.

و المعنظومة المذكورة معظومية لحير غطية ولذلك عم استعتاج لاادون المحتكم لهذه المعنظومة باستعدام طريلة الجذف اللاغطى.

ولد بينت المحاكاة والنتائج لاحالية الطريقة المحترحة فى تصميم نظام التدهم للمنظومة الكهروميكانيكية.

ABSTRACT:

The paper introduces a suggested technique for the design of a nonlinear electromechanical control system. The suggested design is applied to a motor-generator set. This technique electromechanical system is nonlinear and at the same time multivariable. The effect of a nonlinear power amplifier included in the system is also considered. The main objective of such design is to generate electrical power with low harmonic content, which is necessary for the speed control of a.c. motors. Th motor-generator set represents a multivariable system since, it required to control both the frequency and amplitude of the power. The system has also two inputs, the voltage at th terminals and the excitation voltage of the general affects both outputs and hence, decoupling is requir multivariable system. The system is nonlinear by i' hence, a nonlinear approach is used for the design controller. Therefore, the suggested design tech the nonlinear cancellation approach. The pe nonlinear mathematical model of the electry the state space form. A numerical exar illustrate the effectiveness of the desir suggested design technique. Simulation of the electromechanical system v external disturbance on the load s

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INTRODUCTION:

Electromechanical systems are usually exposed to different types of nonlinearities, which affect severely the dynamic performance of such systems. The electro-mechanical system shown in fig. (1) consists of a single phase alternator, driven by an armature controlled d. c. motor. The objective of this work is to design a nonlinear compensator for controlling the frequency and the amplitude of the a.c. power at the output terminals of the single phase alternator. The shown motor-generator set has two inputs, these inputs are the motor armature voltage and the field voltage of the alternator.

MATHEMATICAL MODEL OF THE SYSTEM : the mathematical model of the

system can be represented in state space (1), by the following set of differential equations:

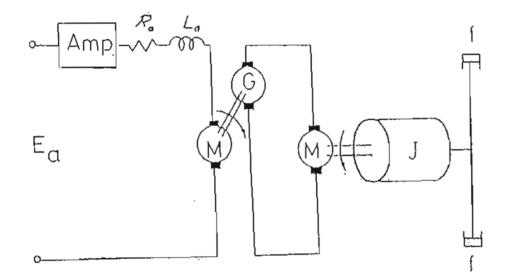


Fig. (1)

$$\dot{\mathbf{x}}_{1} = -\frac{\mathbf{R}_{L}}{\mathbf{L}} \times_{1} + \frac{\mathbf{K}_{g}}{\mathbf{L}} \times_{\sigma} \times_{2}$$
(1)

$$X_{2} = \frac{J_{g}}{J} \times_{z} + \frac{J}{J} \times_{z} - \frac{J_{g}}{J} \times_{z} \times_{z} \times_{z}$$
(2)

$$= K_{g}(x_{4} - x_{2})$$
(3)

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$$\frac{F}{X_{4}} = \frac{F_{m}}{J_{m}} \times_{4} - \frac{1}{J_{m}} \times_{3} + \frac{K_{m}}{J_{m}} \times_{5}$$
(4)

$$\dot{x}_{5} = \frac{r_{a}}{L_{a}} x_{5} - \frac{\kappa_{m}}{L_{a}} x_{4} + \frac{1}{L_{a}} u_{4}$$
(5)

$$x_{\sigma} = -\frac{f}{L} x_{\sigma} + \frac{1}{L} u_{z}$$
(6)

$$y_{1} = R_{L} x_{1}$$
(7)
$$y_{2} = x_{2}$$
(8)

 $x_i = load current,$

x = angular velocity of the generator,

 x_{a} = the torque available to drive the generator,

 x_i = angular velocity of the motor.

 x_{-} = armature current of the motor,

 x_{a} = field current of the generator.

K = shaft stiffness, $r_a^{\circ}, L_a = motor armature resistance and inductance respectively.$

 $R_L, L = local$ resistance and inductance respectively,

 r_{t} , L_{t} = generator field resistance and inductance respectively.

friction coefficient and rotor inertia F,L ≓ viscous respectively, = viscous friction coefficient of the generator of

 F_{q}, J_{q} itsinertia,

 $F_m, J_m = viscous$ friction coefficient of the motor and load inertia,

 K_{a}, K_{m} = generator and motor torque constants respectively,

= input armature voltage to the motor, u_

input field voltage to the alternator. u,

= load voltage, У,

= angular velocity of the generator, У,

Compensator design via nonlinear cancellation:

The model represented by equations (1) \rightarrow (8) can be re-written in the input/output form as follows [2,4] using equations (2), (7) & (8) we can write:

$$y_{2} = -\frac{k_{m}^{2}}{Jr_{a}}y_{2} - \frac{1}{JR_{L}}\frac{y_{1}^{2}}{y_{2}} + \frac{k_{m}}{Jr_{a}}u_{s}$$

multiplying both sides by y_{2} we get

$$y_{2}y_{2} = \frac{k_{m}}{Jr_{a}} y_{2}^{2} - \frac{1}{JR_{L}} y_{i}^{2} + \frac{k_{m}}{Jr_{a}} y_{2}u_{i}$$
(9)

Also, from (7) we have

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