# [Mansoura Engineering Journal](https://mej.researchcommons.org/home)

[Volume 34](https://mej.researchcommons.org/home/vol34) | [Issue 2](https://mej.researchcommons.org/home/vol34/iss2) [Article 8](https://mej.researchcommons.org/home/vol34/iss2/8) Article 8

11-26-2020

# Hybridized Anaerobic Baffled Reactor for the Treatment of Domestic Wastewater: Pilot and Prototype Scale.

A. Badwey Teaching assistant of Environmental Engineering., Mansoura University., Mansoura., Egypt

Ragab Barakat Assistant Professor., Sanitary Engineering., El-Mansoura University., Mansoura., Egypt.

A. Fadel Professor of Sanitary Engineering, Mansoura University., Mansoura., Egypt

Follow this and additional works at: [https://mej.researchcommons.org/home](https://mej.researchcommons.org/home?utm_source=mej.researchcommons.org%2Fhome%2Fvol34%2Fiss2%2F8&utm_medium=PDF&utm_campaign=PDFCoverPages)

#### Recommended Citation

Badwey, A.; Barakat, Ragab; and Fadel, A. (2020) "Hybridized Anaerobic Baffled Reactor for the Treatment of Domestic Wastewater: Pilot and Prototype Scale.," Mansoura Engineering Journal: Vol. 34 : Iss. 2 , Article 8.

Available at:<https://doi.org/10.21608/bfemu.2020.125654>

This Original Study is brought to you for free and open access by Mansoura Engineering Journal. It has been accepted for inclusion in Mansoura Engineering Journal by an authorized editor of Mansoura Engineering Journal. For more information, please contact [mej@mans.edu.eg](mailto:mej@mans.edu.eg).

# Hybridized Anaerobic Baffled Reactor For The Treatment Of Domestic Wastewater: Pilot and Prototype Scale

المفاعلات اللاهو ائيه ذات الحواجز والوسط في معالجة مياه الصر ف الصحي من خلال محطة حقلية و تجر ببية

A. BADWEY \*, R. BARAKAT\*\* and A. FADEL\*\*\*

\* Teaching assistant of Environmental Engineering, Mansoura University.

\*\* Lecturer of Sanitary Engineering, Mansoura University.

\*\*\* Professor of Sanitary Engineering, Mansoura University.

#### المغلامية

المفاعلات اللاهوانيه ذات الحواجز والوسط تتميز على باقي المعالجات اللاهوانيه واعتمادا على ذلك تم تطبيق هذا النظام واستخدامة. ويتميز المفاعل اللاهوائي ذو الحواجز والوسط بقدرته على الفصل بين عمليات تكوين الأحماض و عمليات تكوين غاز الميثان مما يجعل الخزان الواحد بعمل على أنه ّدو مرحلتين بدون زيادة في التكاليف او حدوث اي مشاكل وتم تتفيذ اول محطة معالجة بنظام المفاعلات اللاهوائيه ذات الحواجز والوسط بقرية دمو على بعد ١٠ كم شرق مدينة الفيوم بتصرف ١٦٧٨ م١ بوم وقد تم مراقبتها لمدة عام كامل من اجل تقيع النظم ذات التكلفة المنخفضة التي تلائم ظروف القرى المصرية المنعزلة او ذات الكثافات المنخفضة و أظهرت النتائج أن خواص المياه الناتجة من المحطة كانت اقل من الحدود التي حددها القانون ٤٨ لعام ١٩٨٢. ولكن كفَّاءتها في إزالة الملوثات العضوية والمواد العالقة أقل من كفاءة المحطة التجريبية بقرية نواج حيث كلن متوسط نسب الإزالة للمواد العضوية والمواد العالقة حوالى ٥٠% مقارنة بنسب الإزالة التي حققتها المحطة التجريبية بقرية نواج عند زمن بقاء ٢.٥٠ يوم والتي أعطت متوسط إزالة للمواد العضوية مقداره ١٢ ٨٣% وكان متوسط نسب از الة المواد العالقة ٨٥ ٨٣٨% ويعزى هذا الفارق في كفاءة از الة الملوثات الى عدم ملائمة زمن البقاء المصمم عليه المحطة لخواص مياه الصرف الصحى بقرية دمو

#### Abstract

Hybridized anaerobic baffled reactor has distinct advantages over many other anaerobic treatment processes. Recognition of these advantages has resulted in a broadening application and use of this system. The most significant advantage is, its ability to separate the acidogenes and methanogenes longitudinally down the reactor allowing the reactor to behave as a two phase system without the associated control problems and high cost (Weiland and Rozzi, 1991). The first full scale HABR in Egypt constructed at Demo, (10 Kms east of EL Fayoum city) to treat a wastewater discharge of about 1678  $m<sup>3</sup>/d$ , was monitored for about one year in order to investigate the applicability of this system as a low cost sanitation technology matches the Egyptian village circumstances. Results showed that the full scale HABR achieved an accepted effluent quality corresponds the Egyptian limitations, but the performance was lower than anticipated from the pilot scale HABR constructed at Nawag village. The most frequented removal ratios at HRT of 2.5 days for COD and SS were around 50% for the studied reactors, while the average removal ratios for the pilot plant were 83.12% and 83.58% for COD and suspended solids, respectively at the same HRT.

#### **KEYWORDS**

Hybridized Anaerobic Baffled Reactors (HABR), Chemical Oxygen Demand (COD), Suspended Solids (SS), Hydraulic retention time (HRT).

# **INTRODUCTION**

The successful application of anaerobic technology to the treatment of domestic wastewater depends on the development of high-rate bioreactors such as the upflow anaerobic sludge blanket reactor concepttion (Lettinga et al., 1980), which achieve a high reaction rate per unit reactor volume by retaining the biomass in the reactor for long periods of time. While there have been many high rate designs developed, the anaerobic baffled reactor has many advantages compared to these, such as better resilience to hydraulic and organic shock loads, the ability to partially separate the various phases of anaerobic catabolism and lower sludge yields than many other high rate anaerobic treatment systems. The differing populations of bacteria across the compartments increase resistance  $\mathsf{to}$ variations  $in$ feed load. temperature and pH, (Barber and Stuckey, 1999).

The **HARR** configuration satisfies the main characteristics required for biological treatment systems simple to be and efficient: high biomass a) concentration inside the reactor. cellular propitiating high retention times; b) development  $\alpha$ f structured multi-cellular  $form$ the of aggregates  $in$ dense sludge, granules or composed by different species micro organism groups and responsible for the conversion of organic matter into methane and

carbon dioxide; c) low requirement of nutrients and low excess sludge production:  $\mathbf{d}$ high stability in response to normal fluctuations  $\alpha$ f influent composition and concentration; e) capacity of accommodating high organic loading rates (OLR), (Foresti, 2001).

Construction costs, installations and operation of the HABR are lower than those of conventional aerobic units because the reactor does not require equipment for process maintenance and control. In. fact. the environmental conditions inside the reactor are adequate because anaerobic processes are mainly self controlled. Additionally, the production of excess sludge is minimal and energy balances are quite favorable due to the production of methane. The most significant advantage of the HABR is its ability to separate acidogenesis and methanogenesis longitudinally down the reactor, allowing the reactor to behave as a twophase system without associated control problems and high costs (Weiland and Rozzi, 1991). Two-phase operation increases acidogenic and methanogenic activity by a factor of up to four as acidogenic bacteria accumulate within the first stage (Cohen et al., 1980, 1982), and different bacterial groups can develop under more favorable conditions. The advantages of two-phase operation have been extensively documented by Pohland and Ghosh, 1971, Ghosh et al., 1975 and Cohen et al., 1980, 1982.

Hence, the aim of this research was to evaluate the performance of the full scale HABR plant for treating domestic wastewater by achieved determining the efficiencies  $for$ the removal pollutants. Also. wastewater comparing the full scale with Nawag pilot scale performance.

## **MATERIALS & METHODS** A) Demo full scale plant

Demo, housing and educational complex consists of one hundred house buildings, seventy four constructed the and were remaining twenty six are under construction, in addition to four schools (the secondary school, commercial secondary school, technical secondary school and the handicapped school), also there is a scientific inventions center and a health unit. The area  $\sigma$ Demo complex is a rectangular area reaches 70 feddan, the permanent population is 10000 capita and the total average wastewater discharge is 1678  $m^3/d$ . The HABRs receive settled wastewater from septic tanks via a small bore sewer network consists of (u.P.V.C) pipes ranging in diameters from 4 to 8 inches. The treated effluent from the HABRs is collected again via a network of pipes extended to a 3 m in diameter pump station. At the pump station, the effluent is aerated and disinfected in order be discharged  $b\nu$ two to submersible pumps  $(1+1)$  via a 8 inch force main to the drain 4500 m away from Demo. This system has the advantage that, there is

no definite site combining the treatment plant components, but these components are distributed within the whole area of the complex as shown in figure  $(1)$ . The HABRs were designed to hydraulic achieve  $2.5$ days retention time (HRT). Four large reactors were constructed, and seven existing septic tanks were reformed to be house HABRs. The four large HABRs (1 reactor 750  $m<sup>3</sup>$  and 3 reactors 550  $m<sup>3</sup>$ ) distributed within are the housing area as shown in figure  $(1)$ . The media used in all tanks is plastic with a specific surface area of 80  $m^2/m^3$  and an average depth of 1.0 m as shown in figure  $(2)$ .  $All$ reactors are constructed from reinforced concrete as shown in figure (3). Table (1) shows the summary of the HABRs dimensions.







Fig. (2) Demo HABRs biological media



A. Badawey, R. Barakat and A. Fadel  $C.106$ 

Three HABRs were selected to be studied, in addition the pump station. The sampling points were from the inlet and the outlet of the units except the pump station at which samples were taken from the well. The selected Units are shown in figure  $(1)$  and they are **as** follows:

- $\triangleright$  HABR1 with volume 750 m<sup>3</sup>, which serves part of the 46 house buildings.
- $\triangleright$  HABR2 with volume 550 m<sup>3</sup>. which serves the secondary and commercial secondary schools in addition to the scientific inventions center.
- $\triangleright$  HABR3 with volume 75 m<sup>3</sup>, which serves part of the 8 house buildings.



 $\triangleright$  The pump station.

## B) Nawag pilot plant

Four reactor trains were constructed each with a total volume of 800 liters  $(0.8 \text{ m}^3)$ . Figure  $(4)$ shows section elevation of the pilot plant and its components. To achieve the baffling configuration (compartmentalization), each reactor was constructed from four circular plastic tanks placed in series with a net volume of  $0.2 \text{ m}^3$  per

tank. Each tank had an inner diameter of 55.0 cms and a total depth of 105.0 cms and a net water depth of 85.0 cms, (Khalil,  $2002$ ). Table  $(2)$  gives a brief summary for the reactors configuration. The average influent COD was 300 mg/l and the average SS was 175 mg/l, Various HRT were applied (3.5,  $2.5, 1.5, 1, 0.5$  days.

A. Badawey, R. Barakat and A. Fadel  $C.108$ 

From the analysis of Nawag pilot results. Khalil 2002 plant mentioned that the HRT of 2.5 days was the most suitable and satisfying retention time to be applied, in order to obtain high removal ratios for COD and SS. also HABR with plastic media

achieved the best performance. Finally there was no need for pH or temperature control. Thus, the HABRs of Demo were designed to achieve a HRT of 2.5 days using plastic media according to the recommendations obtained from the pilot study.

Reactor Item		2		
Volume $(m^3)$	0.8	0.8	0.8	0.8
<b>Compartment numbers</b>				
Type of media	Plastic	none	gravel	gravel
Depth of media (m)	0.6		0.3	0.6
Specific surface area $(m^2/m^3)$	100		60-65	
Void ratio (%)	97		$40 - 50$	
Mass/unit volume $\frac{\text{kg}}{\text{m}^3}$	$20 - 25$		1200 - 1400	

Table (2) Details of the pilot plant HABRs of Nawag

Samples were collected from the inlet and outlet of the previous mentioned studied HABRs at Demo and from the inside of the pump station. Samples were according analyzed  $\mathfrak{t}$ the Standard Methods, 1992 in order to measure the chemical oxygen demand suspended  $(COD)$ , solids (SS), pH.

# **RESULTS & DISCUSSION**

This section deals with the discussion of the results obtained from the analysis of Demo samples as well as, comparing its results with Nawag pilot plant results (only with the 2.5 HRT and plastic media HABRs).

# A) COD Removal Ratios

Table  $(3)$ summarizes the achieved COD removal ratios for the different HABRs at Demo. It can be noticed that the average removal values are nearly the same except for HABR2. These values are  $(53.08 \pm 4.53)$ ,  $(30.10)$  $\pm$  10.65), (53.82  $\pm$  5.20) for HABR1. HABR2, HABR3 respectively, while the average COD removal ratio for Nawag plant was  $(83.12 \pm 1.24)$ . The difference between the results of pilot and large scale plants refers mainly to the inconvenient



 $C.109$ 

l,

#### $C.110$ A. Badawey, R. Barakat and A. Fadel

HRT (2.5 days) which is too high for the  $low$ strength wastewater at Demo plant. This is also implemented by the argument that low hydraulic retention times  $(6 - 2)$  hours are feasible during low strength treatment (Orzco. 1988). Confirming such hypothesis, the performance of both building HABRs  $(1, 3)$  is nearly the same while, the schools HABR2 gave a very low performance. Figure (5) shows the COD removal ratios for the studied HABRs while, figures (6) illustrate that

the influent wastewater strength at Nawag is high  $(250-350 \text{ mg/l})$ compared to what found at Demo (Max influent  $COD = 130$ mg/l) due to the presence of septic tanks. HABR2 usually has very low influent and effluent COD and SS values accordingly too removal ratios, because it receives its wastewater from the septic tanks of the secondary schools, these schools work a limited time during the day, as well as some months during the year, so this tank could be omitted











Figure (6) Influent COD values for the HABRs

### **B) SS Removal Ratios**

Table  $(4)$ summarizes the achieved SS removal values for the different HABRs at Demo. It can be noticed that the average removal ratios are close to each other for Demo Plant except for HABR2. These values are (54.49)  $\pm$  5.65), (45.45  $\pm$  5.56), (51.45  $\pm$ 8.27) for HABR1, HABR2, HABR3 respectively, while the average SS removal ratio for Nawag plant was  $(83.58 \pm 2.92)$ . It is logic to have low removal ratios for SS from Demo plant according to the fact that SS

represents the major **COD** fraction in domestic sewage thus. low removal of SS will lead to low removal of COD and vice versa. Figure (7) shows the SS removal ratios for the studied HABRs. It can be noticed that the influent SS concentration at Nawag was high (150-200 mg/l) compared to Demo influent concentrations figures (8). The achieved SS removal of Demo much lower plant  $is$ than anticipated from the previous pilot work experience. This is certainly due to the low SS concentration in the influent.

%SS removal <b>HABR</b>	<b>Average</b>	<b>Standard</b> <b>Deviation</b>	Max	$M_{\rm 1D}$
$\cdots$	54.49	5.65	70.59	40.68
HABR2	24.95	9.65	45.45	5.56
HABR3	51.45	8.27	70.79	31.58
<b>NAWAG</b>	83.58	2.92 <b>We can a my</b>	87.65	78.92

Table (4) SS Removal Ratios for HABRs

 $\Delta \sim 10^4$ 



Figure (7) SS removal ratios for the HABRs





#### C) pH Variations

Table (5) shows the variation of the influent pH for the studied HABRs. The average influent pH was  $(7.27 \pm 0.17)$ ,  $(7.30 \pm$ 0.18),  $(7.28 \pm 0.18)$  for HABR1, HABR2, HABR3 respectively. Table (6) shows the effluent pH variations which were  $(7.25 \pm$ 0.18),  $(7.29 \pm 0.21)$ ,  $(7.31 \pm 0.21)$ 0.16) for HABR1, HABR2, HABR3 respectively. The pH variation range was not tangible and all the values were vibrating around the neutral value making a suitable environment for the

methanogenic bacterial activity. figures  $(9,10)$  show the influent and effluent pH variations for the studied HABRs. With regard to Nawag plant the pH was studied for the reactor along its four compartments. the average influent pH was about 7.25, it was decreased in the first two due compartments  $\mathfrak{t}$ the acidogenic activity and reached about 7.10 and then started to increase again in the last two compartments due the to methanogenic activity till it reached its final value which equals 7.60, (Khalil, 2002).

Influent pH <b>HABR</b>	Average	<b>Standard</b> Deviation	Max	Min
HABR1 --------- <b>A X X X X X X X X</b> ********************* **************************	7.27	0.17	7.60	6.80
ARANGEMENT CONTRACTOR A 4 5 6 6 7 8 9 1 1 2 3 4 5 6 7 8 8 9 8 8 8 8 8 8 8  was print a single to a problem in the book de- <b>BR2</b> <b>*********************</b> ********************** <b>********************</b> ********************** colesce a series a	7.30	0.18	7.70	6.80
HABR3	7.28	0.18	7.60	70

Table (5) Influent pH variations for HABRs

### Table (6) Effluent pH variations for HABRs





Figure (9) Influent pH variations for the studied HABRs





### **Pump Station Results**

### • COD Variations

From table  $(7)$ , the average COD concentration obtained inside the pump station was 42.64  $m\varrho/l$ with standard deviation of 4.44. The mode was equal to 43 mg/l and the median was equal to 43 mg/l, which means that the averages have nearly the same value. The maximum COD concentration

was 53 mg/l and this is also not far from the average value while. the minimum was 34 mg/l. The COD concentration inside the pump station during the study period didn't exceeded (even the maximum value) the Egyptian limitations that organizes the disposal  $\alpha$ f the treated wastewater to the drains, which must not exceed 80 mg/l. Figure (11) shows the COD variation inside the pump station during the field study period.

#### Table (7) COD variations inside the Pump Station





#### Figure (11) COD concentration inside the pump station

### **SS Variations**

Table (8) shows that the average obtained SS effluent concentration inside the pump station was 27.69 mg/l with standard deviation of 3.85. The

mode was equal to 24 mg/l and the median was equal to  $27 \text{ mg/l}$ . The maximum SS concentration was 39 mg/l while, the minimum 22  $mg/l$ . The SS was concentration values are very low if it is compared with the

specification which Egyptian maximum SS limits the concentration in. the treated wastewater not to exceed 50

mg/l. Figure (12) shows the SS concentrations inside the pump station during the study period.







Figure (12) SS concentration inside the pump station

#### $\bullet$  pH Variations

Table (9) shows that the average pH within the pump station was 7.30 with standard deviation of 0.13. The mode and the median have also the same value that equals 7.30. The maximum pH value was 7.6 while, the minimum was 7.10.

According to the Egyptian specifications for the disposal of the treated wastewater to drains, the allowable pH range is between 6.0 and  $9.0.$ The achieved pH is coinciding with the limits. Figure  $(13)$  shows the influent and effluent pH variations along the study period inside the pump station.





#### $C.116$ A. Badawey, R. Barakat and A. Fadel



Figure  $(13)$  pH Variations inside the pump station

#### **CONCLUSIONS**

- The full scale HABR at Demo achieved effluent an wastewater quality cope with the Egyptian standards but, the performance was not as anticipated from the pilot study experience.
- The design HRT of 2.5 days was not the appropriate HRT be applied for Demo to because of the low strength wastewater and the bacterial starvation especially along the compartments last of the HARR<sub>s</sub>
- The maximum achieved COD removal for the large scale HABRs was 61.86%, while the maximum SS removal ratio was 70,59% and in general the most frequented removal ratios for COD and

SS. around 50  $\frac{9}{6}$ were differing from the pilot scale **HABR** which achieved average removal ratio  $\alpha$ <sup> $\epsilon$ </sup> 83.12% and 83.58% for COD and SS respectively.

- The specific surface area of the plastic media used in HABR should be more than 100 m2/m3 according to the results obtained from the pilot plant.
- There was no need for pH control because it was always at the required  $pH$  range  $(6-9)$ .

#### **REFERENCES**

1) American Public Health Association (APHA). (1992). Standard methods for the examination of water and wastewater. 18th Ed., Washington, D.C., USA.

 $C.117$ 

- 2) Barber W. P. and Stuckey D. C. (1999). "The use of the anaerobic baffled reactor (ABR) for wastewater treatment: A Review", Wat. Res. Vol. 33, No. 7, pp. 1559-1578.
- 3) Cohen A., Breure A.M., von Andel J.G. and van Dearsen A., (1982), Influence of Phase Sepration on the Anaerobic Digestion of Glucose, II. Stability and kinetic response to shock loadings, Wat. Res. 16, 449-455.
- 4) Cohen A., Breure A.M., von Andel J.G. and van Deursen A., (1980), Influence of Phase Sepration on the Anaerobic Digestion of Glucose, I. Maximun COD turnover rate during continuous operation, Wat. Res. 14, 1439-1448.
- 5) Eugenio Foresti, Anaerobic  $(2001)$ . Treatment Domestic of Sewage: Established Technologies and 9<sup>th</sup> World Congress on Perspectives, Anaerobic "Anaerobic **Digestion** Conversion for Sustainability", Antwerpen-Belgium.
- 6) Ghosh S., Conrad J.R. and Klass D.L.,  $(1975)$ . Anaerobic Acidogenesis of Sewage Sludge, J. WPCF, 47, 30-45.
- 7) Khalil K. Hassan, 2002, "Hybridized anaerobic baffled reactors for wastewater treatment within small communities in

Faculty Engineering. Egypt", of university, In a partial Mansoura fulfillment for the requirements of the Doctor of philosophy in science.

- 8) Letting G., Van Velsen A.F.M., Hobma S. W., de Zeew W., and Klapwijk A., (1980), Use of Upflow Anaerobic Sludge Blanket (UASB) Concept for Biological Wastewater Treatment, Specially for Anaerobic Treatment. Biotechn. Bioeng., 22, 699-734.
- 9) Orozco A. (1988), "Anaerobic wastewater treatment using an open plug flow baffled low temperature". reactor at 5th International Symposium on Anaerobic Digestion, Bologna, Italy, pp. 759-762.
- 10) Pohland F.G. and Ghosh S., (1971), Development in Anaerobic Treatment Processes. In Biological Waste Treatment, ed. R.P, Canale, Interscience, New York, pp. 85-106.
- 11) Weiland P. and Rozzi A. (1991). "The start-up, operation and monitoring of high-rate anaerobic treatment systems: discussers report", Wat. Sci. Technol. 24, (8), 257-277.